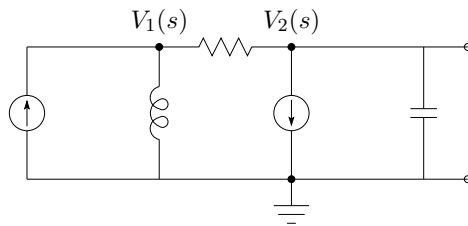


**Node Voltage Analysis:**

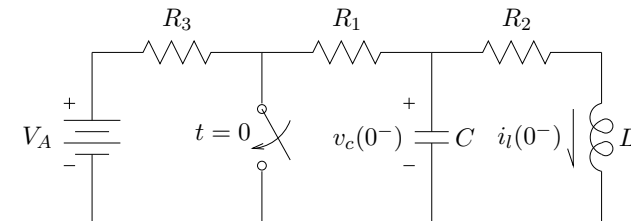
Summary:

1. Find initial conditions (ICs).
2. Transform circuit to  $s$ -domain using *current* sources for ICs. Assign reference and voltage nodes  $\{V_1(s), V_2(s), \dots\}$ .
3. Using KCL at each node, write circuit eqns in terms of  $\{V_1(s), V_2(s), \dots\}$ .
4. Solve eqns (using Cramer's rule, Matlab, etc.).



Notes:

- a) May help to use admittances in step 3 above.
- b) If there are voltage sources, then either ...
  - Assign reference node at one end of the source.
  - Convert to current source using Norton equivalent.
  - Last resort: Define a supernode.

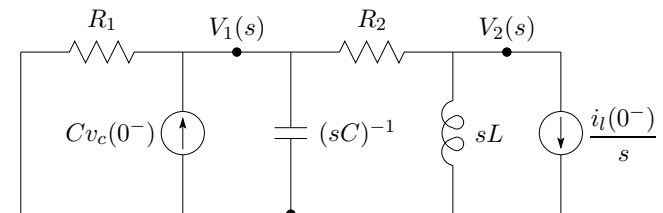
**Example of Node Voltage Analysis:**

- 1) Find initial conditions: (open capacitor, short inductor)

$$i_L(0^-) = \frac{V_A}{R_1 + R_2 + R_3}$$

$$v_c(0^-) = R_2 i_L(0^-) = \frac{V_A R_2}{R_1 + R_2 + R_3}$$

- 2) Transform circuit to  $s$ -domain: (use currents for ICs)



- 3) Use KCL to set up circuit eqns:

$$\text{Node 1 : } \frac{V_1(s)}{R_1} - C v_c(0^-) + \frac{V_1(s)}{(sC)^{-1}} + \frac{V_1(s) - V_2(s)}{R_2} = 0$$

$$\text{Node 2 : } \frac{V_2(s) - V_1(s)}{R_2} + \frac{V_2(s)}{sL} + \frac{i_L(0^-)}{s} = 0$$

Grouping like voltages...

$$\text{Node 1 : } V_1(s) \left( \frac{1}{R_1} + sC + \frac{1}{R_2} \right) + V_2(s) \left( -\frac{1}{R_2} \right) = C v_c(0^-)$$

$$\text{Node 2 : } V_1(s) \left( -\frac{1}{R_2} \right) + V_2(s) \left( \frac{1}{sL} + \frac{1}{R_2} \right) = -\frac{i_l(0^-)}{s}$$

Rewriting in terms of admittances...

$$\text{Node 1 : } V_1(s) (G_1 + sC + G_2) + V_2(s) (-G_2) = C v_c(0^-)$$

$$\text{Node 2 : } V_1(s) (-G_2) + V_2(s) \left( \frac{1}{sL} + G_2 \right) = -\frac{i_l(0^-)}{s}$$

Matrix/vector representation:

$$\begin{bmatrix} sC + G_1 + G_2 & -G_2 \\ -G_2 & G_2 + \frac{1}{sL} \end{bmatrix} \begin{bmatrix} V_1(s) \\ V_2(s) \end{bmatrix} = \begin{bmatrix} C v_c(0^-) \\ -\frac{i_l(0^-)}{s} \end{bmatrix}$$

4) To solve by hand, use Cramer's rule:

$$V_1(s) = \frac{\Delta_1(s)}{\Delta(s)}, \quad V_2(s) = \frac{\Delta_2(s)}{\Delta(s)}$$

where

$$\Delta(s) = \begin{vmatrix} sC + G_1 + G_2 & -G_2 \\ -G_2 & G_2 + \frac{1}{sL} \end{vmatrix}$$

$$\Delta_1(s) = \begin{vmatrix} C v_c(0^-) & -G_2 \\ -\frac{i_l(0^-)}{s} & G_2 + \frac{1}{sL} \end{vmatrix}, \quad \Delta_2(s) = \begin{vmatrix} sC + G_1 + G_2 & C v_c(0^-) \\ -G_2 & -\frac{i_l(0^-)}{s} \end{vmatrix}$$

Calculating determinants...

$$\begin{aligned} \Delta(s) &= \begin{vmatrix} sC + G_1 + G_2 & -G_2 \\ -G_2 & G_2 + \frac{1}{sL} \end{vmatrix} \\ &= (sC + G_1 + G_2) \left( G_2 + \frac{1}{sL} \right) - G_2^2 \\ &= sCG_2 + G_1G_2 + \frac{sC + G_1 + G_2}{sL} \\ &= \frac{s^2LCG_2 + s(LG_1G_2 + C) + G_2 + G_2}{sL} \end{aligned}$$

$$\begin{aligned} \Delta_1(s) &= \begin{vmatrix} C v_c(0^-) & -G_2 \\ -\frac{i_l(0^-)}{s} & G_2 + \frac{1}{sL} \end{vmatrix} \\ &= C \left( G_2 + \frac{1}{sL} \right) v_c(0^-) - \frac{G_2 i_l(0^-)}{s} \end{aligned}$$

$$V_1(s) = \frac{\Delta_1(s)}{\Delta(s)} = \frac{sLC(G_2 + \frac{1}{sL})v_c(0^-) - LG_2 i_l(0^-)}{s^2LCG_2 + s(C + LG_1G_2) + G_1 + G_2}$$

$$\begin{aligned} \Delta_2(s) &= \begin{vmatrix} sC + G_1 + G_2 & C v_c(0^-) \\ -G_2 & -\frac{i_l(0^-)}{s} \end{vmatrix} \\ &= -\frac{i_l(0^-)}{s} (sC + G_1 + G_2) + CG_2 v_c(0^-) \end{aligned}$$

$$V_2(s) = \frac{\Delta_2(s)}{\Delta(s)} = \frac{sLCG_2 v_c(0^-) - L(sC + G_1 + G_2) i_l(0^-)}{s^2LCG_2 + s(C + LG_1G_2) + G_1 + G_2}$$

Plugging in ICs and simplifying...

$$i_l(0^-) = \frac{V_A}{R_1 + R_2 + R_3} = G_2 v_c(0^-)$$

$$v_c(0^-) = \frac{V_A R_2}{R_1 + R_2 + R_3} = \frac{i_l(0^-)}{G_2}$$

$$\begin{aligned} V_1(s) &= \frac{sLC(G_2 + \frac{1}{sL})v_c(0^-) - LG_2 i_l(0^-)}{s^2 LCG_2 + s(C + LG_1 G_2) + (G_1 + G_2)} \\ &= \frac{sv_c(0^-) + \frac{v_c(0^-)}{LG_2} - \frac{i_l(0^-)}{C}}{s^2 + s(\frac{1}{LG_2} + \frac{G_1}{C}) + (\frac{G_1}{LCG_2} + \frac{1}{LC})} \\ &= \frac{s + \frac{1}{LG_2} - \frac{G_2}{C}}{s^2 + s(\frac{1}{LG_2} + \frac{G_1}{C}) + (\frac{G_1}{LCG_2} + \frac{1}{LC})} v_c(0^-) \\ &= \frac{s + \frac{R_2}{L} - \frac{1}{R_2 C}}{s^2 + s(\frac{R_2}{L} + \frac{1}{R_1 C}) + (\frac{R_2}{LCR_1} + \frac{1}{LC})} \cdot \frac{V_A R_2}{R_1 + R_2 + R_3} \end{aligned}$$

$$\begin{aligned} V_2(s) &= \frac{sLCG_2 v_c(0^-) - L(sC + G_1 + G_2)i_l(0^-)}{s^2 LCG_2 + s(C + LG_1 G_2) + (G_1 + G_2)} \\ &= \frac{s(v_c(0^-) - \frac{i_l(0^-)}{G_2}) - \frac{1}{C}(\frac{G_1}{G_2} + 1)i_l(0^-)}{s^2 + s(\frac{1}{LG_2} + \frac{G_1}{C}) + (\frac{G_1}{LCG_2} + \frac{1}{LC})} \\ &= \frac{-\frac{1}{C}(\frac{G_1}{G_2} + 1)}{s^2 + s(\frac{1}{LG_2} + \frac{G_1}{C}) + (\frac{G_1}{LCG_2} + \frac{1}{LC})} i_l(0^-) \\ &= \frac{-\frac{1}{C}(\frac{R_2}{R_1} + 1)}{s^2 + s(\frac{R_2}{L} + \frac{1}{R_1 C}) + (\frac{R_2}{LCR_1} + \frac{1}{LC})} \cdot \frac{V_A}{R_1 + R_2 + R_3} \end{aligned}$$

Did we make a mistake? Verify with Matlab...

```
>> clear all
>> syms s C L R1 R2 R3 V1 V2 VA iL vC
>> iL = VA/(R1 + R2 + R3);
>> vC = VA*R2/(R1 + R2 + R3);
>> syms tmp
>> tmp = inv( [s*C + 1/R1 + 1/R2, -1/R2; -1/R2, 1/R2 + 1/s/L] )...
*[C*vC; -iL/s];
>> pretty(tmp)
```

$$\begin{bmatrix} (sL + R2)R1CVA R2 & R1LVA \\ \hline \%1(R1 + R2 + R3) & \%1(R1 + R2 + R3) \\ R1sLCVA R2 & (sCR1R2 + R2 + R1)LVA \\ \hline \%1(R1 + R2 + R3) & \%1(R1 + R2 + R3) \end{bmatrix}$$

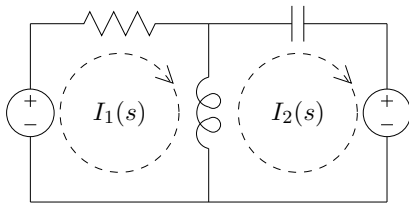
```
2
%1 := s C R1 L + s C R1 R2 + s L + R2 + R1
>> pretty( simplify(tmp) )
```

$$\begin{bmatrix} & 2 & \\ R1VA(CR2sL + CR2 - L) & & \\ \hline 2 & & \\ (sCR1L + sCR1R2 + sL + R2 + R1)(R1 + R2 + R3) & & \\ LVA(R1 + R2) & & \\ \hline 2 & & \\ (sCR1L + sCR1R2 + sL + R2 + R1)(R1 + R2 + R3) & & \end{bmatrix}$$

**Mesh Current Analysis:**

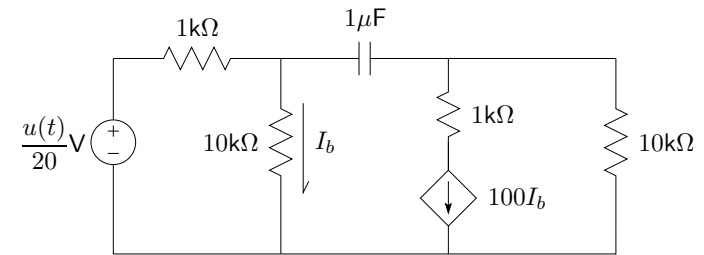
Summary:

1. Find initial conditions (ICs).
2. Transform circuit to  $s$ -domain using *voltage* sources for ICs. Assign mesh currents  $\{I_1(s), I_2(s), \dots\}$ .
3. Using KVL around each loop, write circuit eqns in terms of  $\{I_1(s), I_2(s), \dots\}$ .
4. Solve eqns (using Cramer's rule, Matlab, etc.).

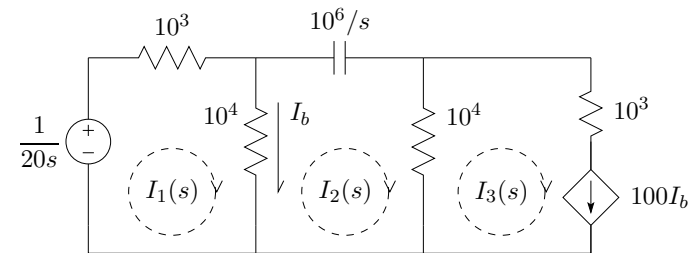


Notes:

- a) Applicable only if the circuit can be drawn on a flat surface without crossovers.
- b) If there are current sources, then either ...
  - Isolate current source in a single mesh current.
  - Convert to voltage source using Thévenin equivalent.
  - Last resort: Define a supermesh.

**Example of Mesh Current Analysis:**Say no energy stored in capacitor for  $t < 0$ :

- 1) Initial currents and voltages equal zero.
- 2) Transforming to  $s$ -domain...



Current source isolated by rearranging circuit:

$$I_3(s) = 100I_b = 100(I_1(s) - I_2(s))$$

Now don't need to solve for  $I_3$  since it's determined by  $I_1$  and  $I_2$ .

3) Use KVL to set up circuit equations:

$$\text{Mesh 1 : } 10^3 I_1(s) + 10^4 (I_1(s) - I_2(s)) - \frac{1}{20s} = 0$$

$$\text{Mesh 2 : } \frac{10^6}{s} I_2(s) + 10^4 (I_2(s) - I_3(s)) + 10^4 (I_2(s) - I_1(s)) = 0$$

Using  $I_3(s) = 100(I_1(s) - I_2(s))$  and collecting like currents. . .

$$\text{Mesh 1 : } I_1(s) (10^3 + 10^4) + I_2(s) (-10^4) = \frac{1}{20s}$$

$$\text{Mesh 2 : } I_1(s) (-10^6 - 10^4) + I_2(s) \left( \frac{10^6}{s} + 10^4 + 10^6 + 10^4 \right) = 0$$

Matrix/vector representation:

$$\begin{bmatrix} 1.1e4 & -1e4 \\ -1.01e6 & \frac{1e^6}{s} + 1.02e6 \end{bmatrix} \begin{bmatrix} I_1(s) \\ I_2(s) \end{bmatrix} = \begin{bmatrix} \frac{0.05}{s} \\ 0 \end{bmatrix}$$

Using Cramer's rule. . .

$$\Delta(s) = \begin{vmatrix} 1.1e4 & -1e4 \\ -1.01e6 & \frac{1e^6}{s} + 1.02e6 \end{vmatrix} = \frac{1.1e10}{s} + 1.12e9 = \frac{1.12e9(s+9.82)}{s}$$

$$\Delta_1(s) = \begin{vmatrix} \frac{0.05}{s} & -1e4 \\ 0 & \frac{1e^6}{s} + 1.02e6 \end{vmatrix} = \frac{5e4}{s^2} + \frac{5.1e4}{s} = \frac{5.1e4(s+0.98)}{s^2}$$

$$\Delta_2(s) = \begin{vmatrix} 1.1e4 & \frac{0.05}{s} \\ -1.01e6 & 0 \end{vmatrix} = -\frac{5.05e4}{s}$$

$$I_1(s) = \frac{\Delta_1(s)}{\Delta(s)} = \frac{(4.55e-5)(s+0.98)}{s(s+9.82)}$$

$$I_2(s) = \frac{\Delta_2(s)}{\Delta(s)} = -\frac{(4.50e-5)}{s+9.82}$$

Using these currents, we can find voltages in circuit. . .

Voltage from top to bottom of left  $10k\Omega$  resistor:

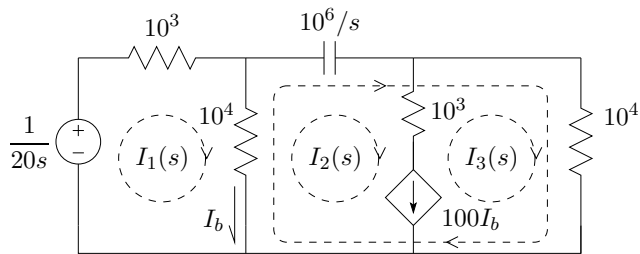
$$V_R(s) = \frac{I_1(s) - I_2(s)}{10^4} = \dots$$

Voltage from left to right across capacitor:

$$V_C(s) = \frac{I_2(s)}{10^6 s^{-1}} = \dots$$

What about the **supermesh** idea?

To see how this works, consider the same circuit but without the dependent source isolated in a single mesh:



The supermesh gives the equations

$$0 = 10^4(I_2(s) - I_1(s)) + \frac{10^6}{s}I_2(s) + 10^4I_3(s)$$

$$I_2(s) - I_3(s) = 100I_b = 100(I_1(s) - I_2(s))$$

So if we plug the second equation into the first to eliminate  $I_3(s)$ ...

$$0 = 10^4(I_2(s) - I_1(s)) + \frac{10^6}{s}I_2(s) + 10^4(101I_2(s) - 100I_1(s))$$

$$= I_1(s)(-10^6 - 10^4) + I_2(s)\left(10^4 + \frac{10^6}{s} + 10^6 + 10^4\right)$$

which is exactly the "Mesh 2" equation we derived earlier!